

## APPENDIX A

% BEGINNING OF PSEUDO CODE

5       % compute scale factor A, and time constants a, b from physical system  
      % parameters

A = Vmax \* Kt / (Re \* Rm + Kt \* Kb) \* l \* k;

10      p1 = 1/Jm/Ie \* (-Ie \* Rm - Re \* Jm + sqrt(Ie^2 \* Rm^2 - 2 \* Re \* Rm \* Ie  
          \* Jm + Re^2 \* Jm^2 - 4 \* Kt \* Kb \* Ie \* Jm)) / 2;  
      p2 = 1/Jm/Ie \* (-Ie \* Rm - Re \* Jm - sqrt(Ie^2 \* Rm^2 - 2 \* Re \* Rm \* Ie  
          \* Jm + Re^2 \* Jm^2 - 4 \* Kt \* Kb \* Ie \* Jm)) / 2;

15      a = max(-p1,-p2)  
      b = min(-p1,-p2)

% make initial guesses for step durations

20      et1 = 1;  
      et2 = .005;  
      et3 = 1;

25      % set maximum iteration count

Nmax = 1000;

for j = 1:Nmax  
      % save old values of step time intervals  
      30      et3old = et3;

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03/04/99



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et2old = et2;
et1old = et1;

% iterate for switch times using fixed voltage level Vmax

5
et3 = -log(1.0 / 2.0 - exp(-et1 * a) / 2 + exp(-et2 * a)) / a;
et2 = 1/b * log(2.0) + 3 * et3 - 1/b * log(2 * exp(1/A * b * X) *
exp(et3 * b) - sqrt( 4.0) * sqrt(exp(1/A * b * X)) * exp(et3 * b)
* sqrt(exp(1/A * b * X)+exp(et3 * b)^2 - 2 * exp(et3 * b)));
et1 = - (-2 * A * et2 + 2 * A * et3 - X) / A;

10
if norm([et3old - et3 et2old - et2 et1old - et1], inf) <= eps * 2
    break
end

15
if j == Nmax
    error(['error - failure to converge after ', num2str(Nmax), '
iterations'])
end

end

20
% round up pulse duration to nearest sample interval,
% convert to intervals between steps to make sure that voltage
% requirements will not increase (beyond Vmax).

25
dt1=ceil((et1 - et2) / dt) * dt;
dt2=ceil((et2 - et3) / dt) * dt;
dt3=ceil((et3) / dt) * dt;

et123 = [et1, et2, et3]

30
% convert back to total step duration.

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et1 = dt1 + dt2 + dt3;

et2 = dt2 + dt3;

et3 = dt3;

5 % In the following, the original constraints equations involving XF1, XF2, % and XF3 have been modified to include a variable voltage level applied at % each step (instead of the fixed maximum (+/-) Vmax).

% The original equations for XF1, XF2, and XF3 follow:

10 %  $XF_1(t_{end}) = V_0 F_1(t_{end} - t_0) - 2V_0 F_1(t_{end} - t_1) + 2V_0 F_1(t_{end} - t_2)$

%  $XF_2(t_{end}) = V_0 F_2(t_{end} - t_0) - 2V_0 F_2(t_{end} - t_1) + 2V_0 F_2(t_{end} - t_2)$

%  $XF_3(t_{end}) = V_0 F_3(t_{end} - t_0) - 2V_0 F_3(t_{end} - t_1) + 2V_0 F_3(t_{end} - t_2)$

% And the modified equation including adjustable relative levels of voltage

15 % L1, L2 and L3 are:

%  $XF_1(t_{end}) = L_1 V_0 F_1(t_{end} - t_0) - L_2 V_0 F_1(t_{end} - t_1) + L_3 V_0 F_1(t_{end} - t_2)$

%  $XF_2(t_{end}) = L_1 V_0 F_2(t_{end} - t_0) - L_2 V_0 F_2(t_{end} - t_1) + L_3 V_0 F_2(t_{end} - t_2)$

%  $XF_3(t_{end}) = L_1 V_0 F_3(t_{end} - t_0) - L_2 V_0 F_3(t_{end} - t_1) + L_3 V_0 F_3(t_{end} - t_2)$

20 % And the corresponding constraint equations are:

%  $XF_1(t_{end}) = Finalpos$

%  $XF_2(t_{end}) = 0$

%  $XF_3(t_{end}) = 0$

25 % Where all of the times indicated have discrete values, e.g. corresponding to % the controller update rate.

% It should be noted that after the digital switch times are fixed, the constraint % equations derived from the equations above form a linear set of equations in % the unknown relative voltage levels L1, L2 and L3 and any standard linear

% method can be used to solve for the relative voltage levels. In the equations  
% for (L1, L2 and L3) that follow, the solution was obtained by algebraic  
% means (and are not particularly compact.)

5       % compute new relative voltage step levels  
% L1, L2 and L3 are nominally assigned to "1", "-2" and "+2", respectively

s1 = X \* (exp(-et3 \* b) \* exp(-et2 \* a) + exp(-et3 \* a) + exp(-et2 \* b) -  
  exp(-et2 \* b) \* exp(-et3 \* a) - exp(-et2 \* a) - exp(-et3 \* b));  
10      s2 = 1 / (et2 \* exp(-et1 \* b) \* exp(-et3 \* a) + exp(-et2 \* b) \* et3 \*  
  exp(-et1 \* a) - et2 \* exp(-et3 \* a) - et2 \* exp(-et1 \* b) - et3 \*  
  exp(-et1 \* a) - exp(-et2 \* b) \* et3 + exp(-et3 \* b) \* et1 \* exp(-et2 \* a)  
  + exp(-et3 \* a) \* et1 + exp(-et2 \* b) \* et1 - exp(-et2 \* b) \* et1 \*  
  exp(-et3 \* a) - et3 \* exp(-et1 \* b) \* exp(-et2 \* a) - exp(-et2 \* a) \* et1 -  
15      exp(-et3 \* b) \* et1 - exp(-et3 \* b) \* et2 \* exp(-et1 \* a) + et3 \*  
  exp(-et1 \* b) + et2 \* exp(-et1 \* a) + exp(-et3 \* b) \* et2 + et3 \*  
  exp(-et2 \* a)) / A;

L1 = s1 \* s2;  
20  
s1 = 1 / (et2 \* exp(-et1 \* b) \* exp(-et3 \* a) + exp(-et2 \* b) \* et3 \*  
  exp(-et1 \* a) - et2 \* exp(-et3 \* a) - et2 \* exp(-et1 \* b) - et3 \*  
  exp(-et1 \* a) - exp(-et2 \* b) \* et3 + exp(-et3 \* b) \* et1 \*  
  exp(-et2 \* a) + exp(-et3 \* a) \* et1 + exp(-et2 \* b) \* et1 -  
25      exp(-et2 \* b) \* et1 \* exp(-et3 \* a) - et3 \* exp(-et1 \* b) \*  
  exp(-et2 \* a) - exp(-et2 \* a) \* et1 - exp(-et3 \* b) \* et1 - exp(-et3 \* b) \*  
  et2 \* exp(-et1 \* a) + et3 \* exp(-et1 \* b) + et2 \* exp(-et1 \* a) +  
  exp(-et3 \* b) \* et2 + et3 \* exp(-et2 \* a)) \* X;  
s2 = (exp(-et2 \* b) \* exp(-et1 \* a) - exp(-et1 \* a) - exp(-et2 \* b) -  
30      exp(-et1 \* b) \* exp(-et2 \* a) + exp(-et1 \* b) + exp(-et2 \* a)) / A;

L3 = s1\*s2;

s1 = exp(-et1 \* a) - exp(-et3 \* a) + exp(-et3 \* b) - exp(-et1 \* b) -  
exp(-et3 \* b) \* exp(-et1 \* a) + exp(-et1 \* b) \* exp(-et3 \* a);

5 s2 = X / (et2 \* exp(-et1 \* b) \* exp(-et3 \* a) + exp(-et2 \* b) \* et3 \*  
exp(-et1 \* a) - et2 \* exp(-et3 \* a) - et2 \* exp(-et1 \* b) - et3 \*  
exp(-et1 \* a) - exp(-et2 \* b) \* et3 + exp(-et3 \* b) \* et1 \* exp(-et2 \* a)  
+ exp(-et3 \* a) \* et1 + exp(-et2 \* b) \* et1 - exp(-et2 \* b) \* et1 \*  
exp(-et3 \* a) - et3 \* exp(-et1 \* b) \* exp(-et2 \* a) - exp(-et2 \* a) \* et1 -  
exp(-et3 \* b) \* et1 - exp(-et3 \* b) \* et2 \* exp(-et1 \* a) + et3 \*  
exp(-et1 \* b) + et2 \* exp(-et1 \* a) + exp(-et3 \* b) \* et2 + et3 \*  
exp(-et2 \* a)) / A;

L2 = s1 \* s2;

15

% convert accumulated voltage steps to sequential voltage level

V1 = Vmax \* (L1);

V2 = Vmax \* (L1 + L2);

V3 = Vmax \* (L1 + L2 + L3);

20

% END OF PSEUDO CODE